

# Autonomous Navigation for KaNaRiA: A Mission into the Asteroid Main Belt

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### KaNaRia

 KaNaRiA = Kognitionsbasierte autonome Navigation am Beispiel des Ressourcenabbaus im All









# Navigation for KaNaRiA

#### NAVIGATION

#### LEADING PROFESSOR



Univ.-Prof. Dr.-Ing. habil. **B. Eissfeller** 

#### **RESEARCH ASSOCIATE**



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#### Navigation and Instrumentation



#### Spacecraft Orbit Determination (OD)

- Concept for precise on-board orbit determination
- Autonomous absolute positioning in space
- Position and attitude filtering strategies

#### Inertial and Relative Navigation

- Concept for precise asteroid-relative navigation
- Development of a **navigation transfer strategy** from **absolute to relative** navigation

#### Spacecraft Instrumentation

- Selection of **optical**, laser, inertial and radar sensors and study of theirs suitability for the asteroid mission KaNaRiA
- Asteroid orbit determination and dynamic characterization from flight observation



# Outline

- KaNaRiA mission scenario
- Navigation requirements
- Navigation system design
- Optical Sun Doppler Navigation (OSDN)



### KaNaRiA: The mission



A. Probst et al. Reference Mission Scenario Selection for Main Belt Asteroid Mining Missions. PTMSS Proceedings. Montreal, May 2015.

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ISTA

### KaNaRiA: The mission







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## Navigation Requirements: Cruise Phase

• 3D orbit determination (OD) error for PTCM < 100 km

PTCM deployment in Parking Orbi

 OD shall be performed autonomously onboard ensuring the required accuracy for a the complete transfer (3-4 years)

 Ground-based OD aid with a maximum tracking interval of 1 week/5 months



### Navigation Requirements: Rendezvous

- The PTCM shall be targeted to a B-plane aim point between 100-500 km from the asteroid surface
- The 3-sigma error ellipsoid at rendezvous condition shall be constraint to 100 m



Source: ESA



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# Navigation Requirements: In-Orbit Phase

from asteroid characterization objectives

Vertical positioning ~1 m

- Horizontal positioning ~ 0.5 m
- Vertical & Horizontal velocity ~ 1 cm/s







Shape model of asteroid 2008 EV5 showing the gravitational slopes. Credits: Marco-Polo-R consortium. Radar tomography schematic. Herique et al. 2006



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# Navigation Requirements: Landing

- <u>Soft landing of a legged structure:</u>
  - Touchdown vertical velocity < 1 m/s</li>
  - Touchdown horizontal velocity < 0.5 m/s</li>
  - Touchdown angle rates < 1 deg/s</li>
- <u>Safe landing</u> (site slopes < 10 deg; biggest site hazards 10 – 50 cm)
  - Pin-point landing accuracy < 5 m
- <u>Autonomy</u> Hazard Detection and Avoidance (HDA)
  - Detection of unmapped hazards > 50 cm within 5 m of target landing site
  - Online planning of new landing trajectory/avoidance manoeuvre within 10 minutes from touchdown





# Navigation System Design





### Optical Sun Doppler Navigation (OSDN) The concept

#### **Sun Direction**



#### **Optical Sun Doppler Shift**



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#### Optical Sun Doppler Navigation (OSDN) Observation Model (1/2)

Radial velocity v<sub>r</sub> derived from Sun Doppler measurements:

$$r \equiv v \downarrow r = \mathbf{r} \cdot \mathbf{r} / r = \mathbf{r} \cdot \mathbf{v} / r$$

• Sun line-of-sight unit vector (being r = rl):

$$l = \cos\theta \cos\phi \, n l \mathbf{1} + \cos\theta \sin\phi \, n l \mathbf{2} + \sin\theta \, n l \mathbf{3}$$
with

$$r = \sqrt{x} \hat{1} 2 + y \hat{1} 2 + z \hat{1} 2 \qquad \theta = \tan \hat{1} - 1 (y/z)$$
  
$$\phi = \sin \hat{1} - 1 (z/r)$$

- Elevation angle,  $\theta$ 

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## Optical Sun Doppler Navigation (OSDN)

Observation Model (2/2)

• Line-of-sight unit vector to a planet, as derived from a CCD camera:

 $l \downarrow P \downarrow i = \cos\theta \downarrow P \downarrow i \cos\phi \downarrow P \downarrow i n \downarrow \mathbf{1} + \cos\theta \downarrow P \downarrow i$  $\sin\phi \downarrow P \downarrow i \mathbf{n} \mathbf{l} \mathbf{2} + \sin\theta \downarrow P \downarrow i \mathbf{n} \mathbf{l} \mathbf{3}$ 

#### with

# $r \downarrow P \downarrow i = \sqrt{x} \downarrow P \downarrow i \uparrow 2 + y \downarrow P \downarrow i \uparrow 2 + z \downarrow P \uparrow 2 \downarrow i$ $r \downarrow P \downarrow i = r \downarrow P \downarrow i \downarrow P \downarrow i$

 $\begin{array}{c} \theta \downarrow P \downarrow i = \tan 1 - 1 \left( \gamma \downarrow P \downarrow i - \gamma / z \downarrow P \downarrow i - z \right) \\ \varphi \downarrow P \downarrow i = \sin 1 - 1 \left( z \downarrow P \downarrow i - z / r \downarrow P \downarrow i - z \right) \\ \varphi \downarrow P \downarrow i = \sin 1 - 1 \left( z \downarrow P \downarrow i - z / r \downarrow P \downarrow i - r \right) \end{array}$ 

#### Optical Sun Doppler Navigation (OSDN) Observables



Parking Orbit	
Semi-major axis	2.8 AU
Eccentricity	0.033
Inclination	5 deg



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# Optical Sun Doppler Navigation (OSDN)



• Power flux from Jupiter:  $\sim 1-0.1 \,\mu W/m^2$  @ parking orbit



#### Optical Sun Doppler Navigation (OSDN) Observables



• Chord length of Jupiter: 0.9-0.04 deg @ parking orbit



#### Optical Sun Doppler Navigation (OSDN) Dynamic Model

• Spacecraft dynamic model, f(x,t):

• 2-body problem with the Sun as central body

r = v

$$r = -\mu ls / rt3 r$$

- Extension to third-body perturbations:
  - Planets or asteroids at fly-by

### $r = -\mu \downarrow s / r \uparrow 3 r - \sum i \uparrow \equiv \mu \downarrow P i / r \downarrow i \uparrow 3 r \downarrow i$



### **Optical Sun Doppler Navigation (OSDN)**

State estimation

- Sequential estimators:
  - Extended Kalman Filter
  - Particle filter



- Sun-relative geometry variations of 0.25° per day in parking orbit
- On-going work:
  - filter tuning
  - measurement frequency set-up
  - LOS occultations







# Thank you!



